

# *The OECD-BSAF Project: The Spanish Involvement*

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Unit of Nuclear Safety Research

CSN (Madrid), Jan. 15<sup>th</sup>, 2015

# *BACKGROUND*



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- **CIEMAT and CSN closely collaborate on severe accident research.**
- **A number of issues have been/are being addressed:**
  - *Fission products retention in meltdown SGTR sequences* (ARTIST).
  - *Fuel degradation in SFP under complete LOCA conditions* (OECD-SFP).
  - *Hydrogen distribution in containment* (OECD-HYMER).
  - *In-Containment Source Term (iodine chemistry)* (PHEBUS-FP).
  - *Pool scrubbing* (EU-PASSAM).
  - *Spanish NPP modeling with the MELCOR code.*
  - *Uncertainty analysis in severe accident simulations.*
- **The Fukushima accidents analyses** (OECD-BSAF)



## THE OECD-BSAF PROJECT



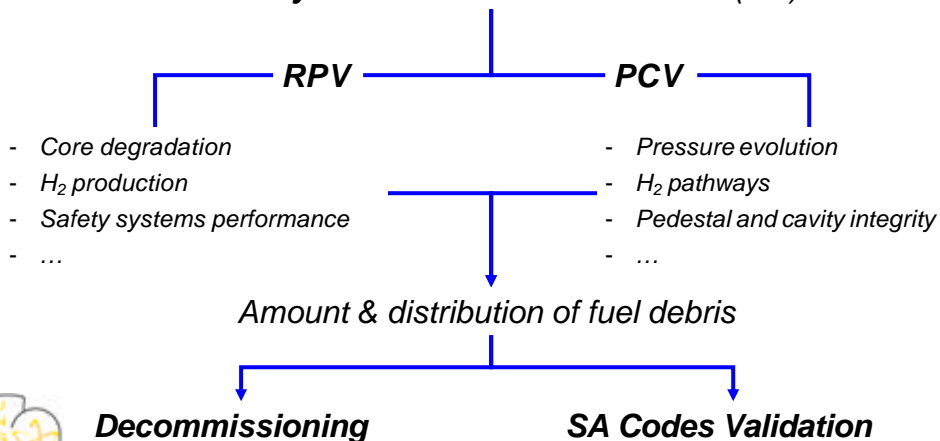
## Overall Description

- **Restricted-participation project under the frame of the OECD-NEA.**
- **A 2-year project:** Nov. 2012 – 2014.
- **Operating agent:** JAEA in collaboration with IAE, JNES, CRIEPI and supported by TEPCO.
- **Participant countries:** France, Germany, Japan, Rep. Of Korea, Russian Fed., Spain, Switzerland and USA.



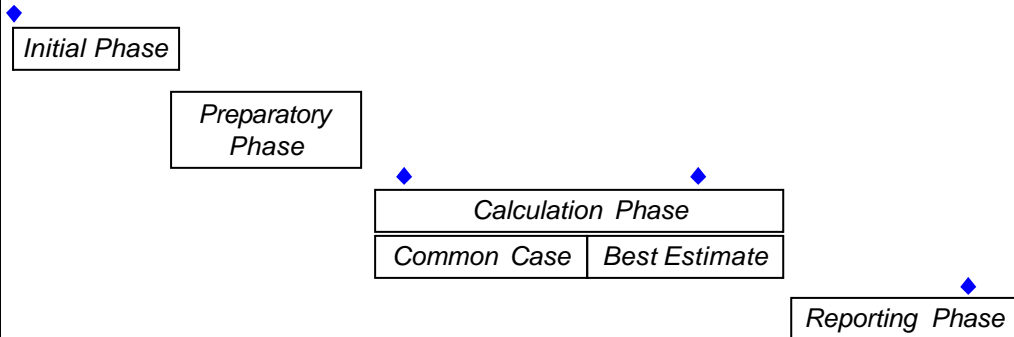
## Objectives & Scope

### TH analysis of 1F1 – 1F3 Accidentes (6 d)



# Project Unfolding

11.12      03.13      09.13      08.14      12.14



# Current Status

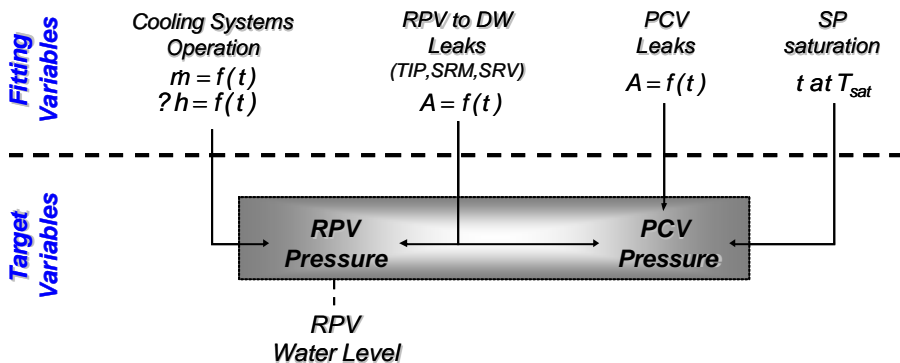
- **Final reporting OECD-BSAF** Jan. – March 2015
- **Discussion of OECD-BSAF II** Jan. – March 2015
  - 3-year project.
  - Technical focus:
    - a. Distribution of FPs and contaminated debris in the units.
    - b. Evaluation of source term
    - c. Review of OECD-BSAF I modeling
  - Time span of analyses: 21 days



# THE CSN-CIEMAT CONTRIBUTION



## Approach

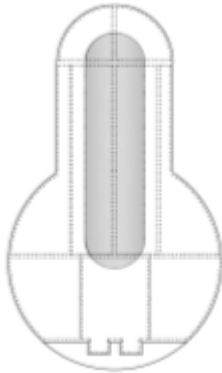


**A number of "feasible" scenarios in each unit**





# Generic Plant Modeling: PCV Nodalisation

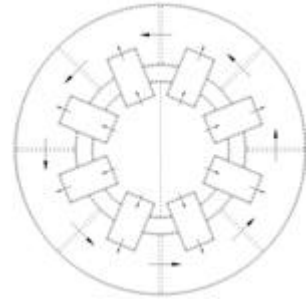


**DW**

**WW**

	DW	WW	Vents	VBs
CVs	9	8	8	-
FLs	16	8	8	8

Volume	1F1	1F2	1F3
DW (m <sup>3</sup> )	3000	3770	3770
WW (m <sup>3</sup> ) (pool)	4370 (1750)	6140 (2980)	6140 (2980)



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# Boundary Conditions

		1F1	1F2	1F3
<b>Power [MW<sub>th</sub>]</b>		1380	2381	2381
<b>Systems</b>	IC	<input checked="" type="checkbox"/>	-	-
	RCIC	-	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
	HPCI	-	-	<input checked="" type="checkbox"/>
	SRV	<input checked="" type="checkbox"/> (4; 1 on)	<input checked="" type="checkbox"/> (8; 1 on)	<input checked="" type="checkbox"/> (8; 1 on)
	Sprays <sub>PCV</sub>	-	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
<b>Venting</b>		<input checked="" type="checkbox"/> (1)	-	<input checked="" type="checkbox"/> (6)
<b>External Water Injection</b>		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
<b>Torus Room</b>		Dry	Flooded	Dry



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## Systems Modeling

- **Systems (IC, RCIC, HPCI):** Modeled "to effect" (i.e. source/sink)
- **Systems (SRV):** Nominal setpoints
  - Relief mode bf. SBO
  - Safety mode af. SBO
- **RPV leakages:** Best fit
- **PCV leakages:** Best fit
- **PCV ventings:** Best fit ( $t$  [s] &  $A$  [ $m^2$ ])
- **External water injections:** Best fit ( $t$  [s] &  $m$  [kg/s])

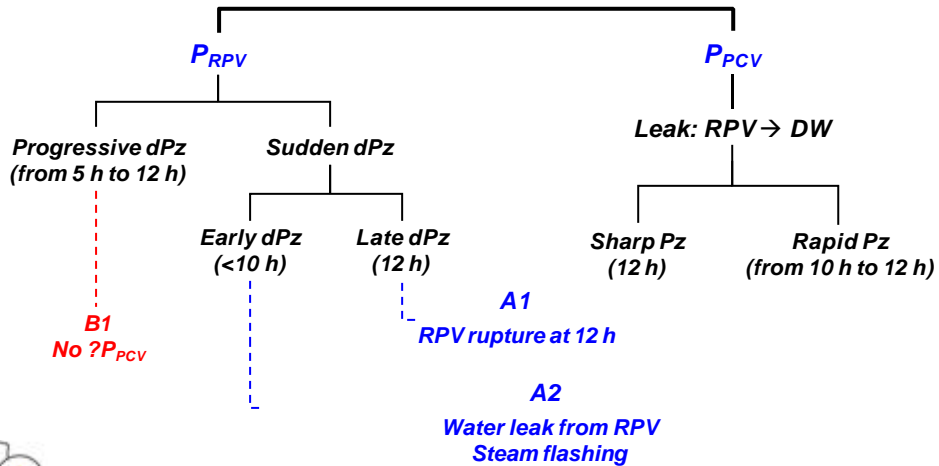


## Phenomena-Related Approximations

- Default values in Flow Paths definition.
- No specific model for eutectic formation.
- Simplified  $B_4C$  oxidation model.
- One-layer model for molten material in cavity.
- The recirculation loop not modeled.
- HPCI & RCIC exhaust modeled as sources in the WW pool ( $h_{steam}$ ).



## Strategy of Pre-Analysis



## Matrix of Scenarios

RPV failure									
Type	SRV <sub>gasket</sub>		CORE <sub>SRM/IRM/TIP</sub>			LP <sub>leak</sub>		SRV <sub>failedOpen</sub>	
	N	Y	N	1-Ring	4-Rings	N	Y	N	Y
1		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
2		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
3		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
4		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	
5	<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	
6	<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>
7	<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	

A1

A2



## Specific Approximations

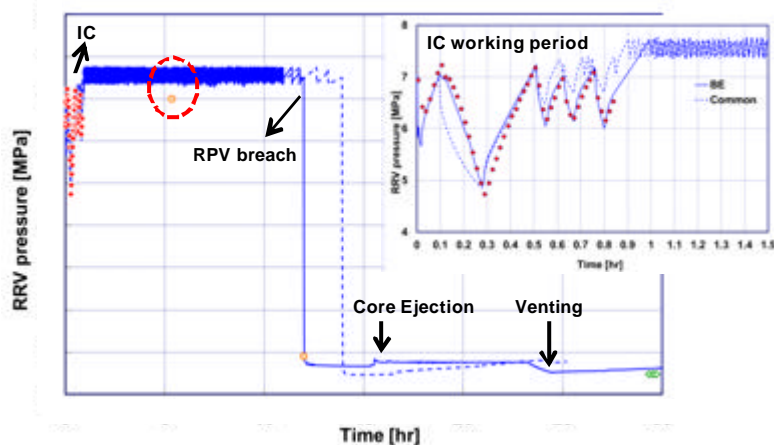
<b>RPV:</b>	<b>IC</b>	Energy sink in dome	BE: adjusted to follow $P_{RPV}$
	<b>Water inj.</b>	Source to downcomer	BE: adjusted to follow $P_{PCV}$
	<b>SRVs</b>	Relief mode (bf. SBO) Safety mode (af. SBO)	$P_{open} / P_{close} : 7.38 / 7.01 \text{ MPa}$ $P_{open} / P_{close} : 7.75 / 7.36 \text{ MPa}$
	<b>"RPV Leaks"</b>	From RPV to DW (SRV gasket)	BE: $T > 723 \text{ K}$ ; $A = 32.6 \cdot 10^{-4} \text{ m}^2$

<b>PCV:</b>	<b>Venting</b>	WW $\rightarrow$ Environment	BE: $t = 23.2 - 24.4 \text{ h}$ ; $A = 0.016 \cdot A_{tot}$ $t > 24.4 \text{ h}$ ; $A^* = 0.14 - 0.02 \cdot A_{tot}$
	<b>DW flange failure</b>	DW $\rightarrow$ Environment	BE: $P > 0.75 \text{ MPa}$ ; $A = f(P)$



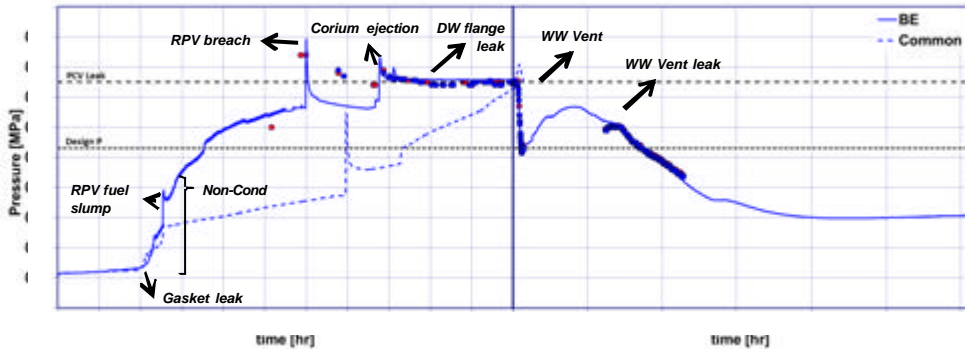
## Results (I)

### RPV Pressure



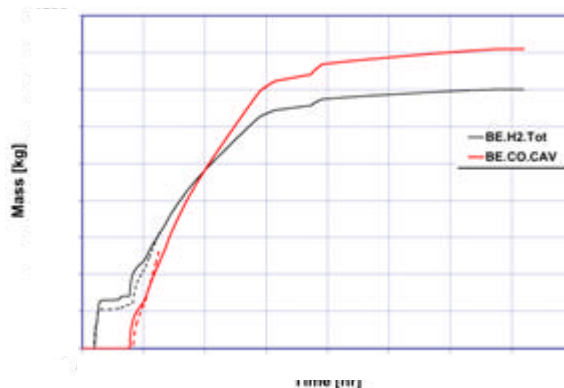
## Results (II)

### PCV Pressure



## Results (III)



### H<sub>2</sub> & CO Generation



# Results (IV)









## Mass Distribution

“Best Estimate”  
 “Common Case”

Solid color columns   
 Stripped color columns 

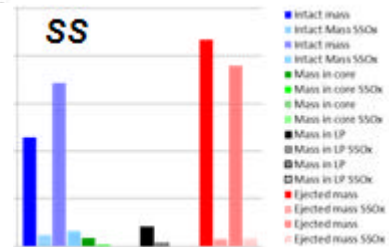
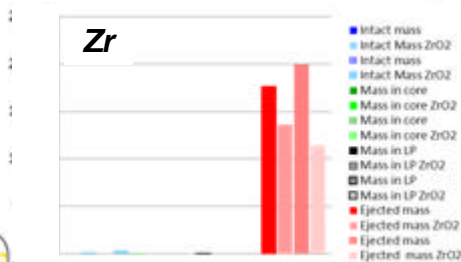
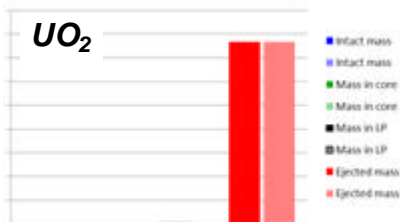
### The Color code

(Zr/SS Oxides)

Intact mass		
Degraded in-core		
Degraded in-LP		
Ejected mass		



# Results (IV)



## Major Insights

- **Final status of 1F1:**
  - Massive core degradation.
  - RPV failed in the first 12 h.
  - Most core materials slumped into the cavity.
  - More than 7000 kg of H<sub>2</sub> & CO (most from MCCI).
- **Detailed evolution of 1F1 highly uncertain! – No proper BE**
  - RPV and PCV data inconclusive.
  - Multiple RPV scenarios feasible.
  - Suppression pool thermal stratification might play a role.



- **“BE cases” is probably not the right way to call them!**
- **“BE scenarios” are highly uncertain.**
  - Boundary conditions ? Scarcity of data to set cross-correlations.
  - Modeling (physical & scenarios) ? Enhancement indispensable!
- **Major modeling uncertainties come from:**
  - Cavity modeling (1F1).
  - Containment modeling (i.e., SC nodalization)



- **“BE Scenarios” vs. “Common Case”:**
  - Consistency in major accident signatures.
  - Substantial differences in some variables unfolding.
- **“BE Insights”:**
  - 1F1 - Core massively degraded and poured into PCV cavity.  
More than 7000 kg of  $H_2 + CO$  generated.  
Potential for liner failure.
  - 1F2 - Half of the core in LP; no RPV failure predicted.  
About 600 kg of  $H_2$  generated.
  - 1F3 - Half of the core relocated in LP; no RPV failure.  
More than 1000 kg of  $H_2$  generated.



- **Refined “BE cases” being calculated.**

**Thank you for your attention!**

**Any questions?**

